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ANALYSIS OF THE PM MOTOR WITH EXTERNAL ROTOR FOR DIRECT DRIVE OF ELECTRIC WHEELCHAIR

The paper deals with analysis of properties of synchronous motor with external permanent magnets rotor. The mathematical analysis and equivalent circuit of permanent magnet synchronous motor (SMPM) is presented. In the parts of the paper the electromagnetic design, construction design and FEM Simulation of a SMPM is described and its properties are analysed. In the paper the results of simulation in Matlab/Simulink of torque, speed and current on the base mathematical model are shown.

Keywords: direct drive, electric vehicle, external rotor, permanent magnet machine, synchronous motor, wheelchair

1. Introduction

Due to some of its advantageous features, such as high efficiency, high torque-to-current ratio, low noise, and robustness has permanent magnets synchronous motor (PMSM) received widespread acceptance in industrial applications [1]. Electric machines present main parts of the electric vehicle power train, whilst demands for electric machines differ. In general, characteristics as large torque, high rotation speed, high power density, quick response and good reliability are in high demand. Synchronous machines supplied by electronic converter are first of all widely used as the permanent magnet synchronous machine in variable speed drives and applied to small electric vehicles [2].

The manufacturers produce small electric vehicles with various types of drives. Drives of small electric vehicles are nowadays the subject of research of many manufacturers and institutes [3]. Design solutions bring several alternatives that differ in technical parameters [4]. Most of the parameters of drive depend directly on design solutions of the electric motor, on its power, battery voltage, dimensions of frequency converter and others. The development of high-quality permanent magnet materials in commercial production has encouraged several manufacturers to introduce various PMSM to the market.

The most practical for the electric wheelchair is a direct drive that is a motor with an external rotor using permanent magnets in-wheel operation. The drive can be designed with an inverse DC motor with permanent magnets or an AC synchronous motor with permanent magnets an external rotor, respectively. Optimal design of synchronous motor parameters is influenced by utilization of inverters [5-6]. The study [7] examines the effects of motor parameters on the torque and speed capability.

The characteristics of a permanent magnet machine are highly dependent on the rotor structure. The rotor can be implemented in various ways. When employing modern permanent magnet materials, the rotor can be constructed even completely without iron.

Designed and produced for direct drive of the wheelchair has been the prototype of an inverse AC synchronous motor with

permanent magnets [8] and this motor is assessed and simulated in the following parts of the paper.

2. Mathematical analysis and equivalent circuit of permanent magnet synchronous motor

As to the modelling, it is common practice to transform all variables from the three-phase system (abc) to an orthogonal (dq) reference frame with a direct (d) and quadrature (q) axis (see Figure 1), where X represents the voltage, current or magnetic flux and θ_r is the rotor angle.

Clarke Transformation $abc \rightarrow \alpha\beta$, see Equation (1), and Park Transformation $\alpha\beta \rightarrow dq$, see Equation (2), can be applied regarding reference frame theory.

$$\begin{bmatrix} \alpha \\ \beta \end{bmatrix} = \frac{2}{3} \cdot \begin{bmatrix} 1 & \cos(2\pi/3) & \cos(4\pi/3) \\ 0 & \sin(2\pi/3) & \sin(4\pi/3) \end{bmatrix} \cdot \begin{bmatrix} a \\ b \\ c \end{bmatrix}, \quad (1)$$

$$\begin{bmatrix} d \\ q \end{bmatrix} = \begin{bmatrix} \cos(\theta_r) & \sin(\theta_r) \\ -\sin(\theta_r) & \cos(\theta_r) \end{bmatrix} \cdot \begin{bmatrix} \alpha \\ \beta \end{bmatrix}. \quad (2)$$

The transformation of a three-phase quantity in abc-coordinate system to dq-system is called Clarke-Park's Transformation. Written in matrix form, see Equation (3), the Clarke-Park's Transformation is defined as

$$\begin{bmatrix} d \\ q \end{bmatrix} = \frac{2}{3} \cdot \begin{bmatrix} \cos(\theta_r) & \cos(\theta_r - 2\pi/3) & \cos(\theta_r + 2\pi/3) \\ \sin(\theta_r) & \sin(\theta_r - 2\pi/3) & \sin(\theta_r + 2\pi/3) \end{bmatrix} \cdot \begin{bmatrix} a \\ b \\ c \end{bmatrix}, \quad (3)$$

Permanent magnet synchronous motors (PMSM) are usually modelled in the rotor reference frame, i.e. in the Clarke-Park's d-q model. In this synchronous reference frame, the PMSM with PM rotor is generally described by the following set of equations [8-9]:

$$u_d = R \cdot i_d + L_d \cdot \frac{di_d}{dt} - \omega L_q i_q, \quad (4)$$

$$u_q = R \cdot i_q + L_q \cdot \frac{di_q}{dt} - \omega L_d i_d + \omega \psi_{Md}. \quad (5)$$

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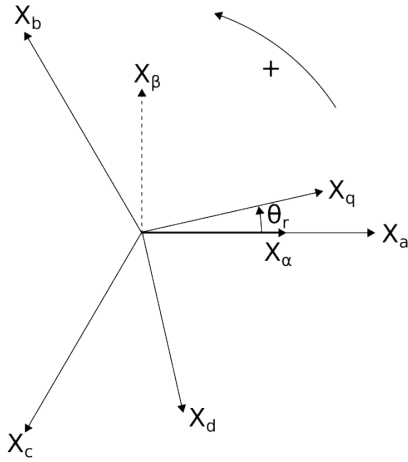


Figure 1 Rotating reference frames

where: u_d and u_q are the d and q axes voltages,
 i_d and i_q are the d and q axes currents,
 R is the stator resistance,
 ω is the electrical angular speed,
 Ψ_{Md} is the permanent magnet flux,
 L_d and L_q are inductances of the stator d and q axes.

The PMSM can be described in Equation (4) and (5) with the following assumptions:

- saturation is negligible,
- the induced back EMF is sinusoidal,
- eddy currents and hysteresis losses are negligible,
- no field current dynamics,
- no cage on the rotor.

The electromagnetic torque can be expressed as follows:

$$T_{em} = \frac{3}{2} \cdot \frac{P}{2} \cdot [\Psi_{Md} \cdot i_d - (L_q - L_d) \cdot i_d \cdot i_q]. \quad (6)$$

where P is the number of poles, i_d and i_q are the d-axis and q-axis components of the stator current vector. Thus, the magnitude of I_s is given by equation:

$$I_s = \sqrt{i_d^2 + i_q^2}. \quad (7)$$

The equivalent circuit of the PM machine shown in Figure 2 is similar to the one for the synchronous machine.

The permanent magnet is modelled by a current source i_m parallel to the resistance R_M . In the magnetizing inductance, this current source produces the permanent magnet's share of the air gap flux linkage:

$$\Psi_{Md} = i_m \cdot L_{md}. \quad (8)$$

However, due to the saturation the magnetizing inductance L_{md} and i_m are not constant. The flux linkage components in Figure 2 are determined by the equations:

$$\Psi_d = i_d \cdot L_d + \Psi_{Md} = i_d \cdot (L_{ld} + L_{md}) + \Psi_{Md}, \quad (9)$$

$$\Psi_q = i_q \cdot L_q = i_q \cdot (L_{lq} + L_{mq}). \quad (10)$$

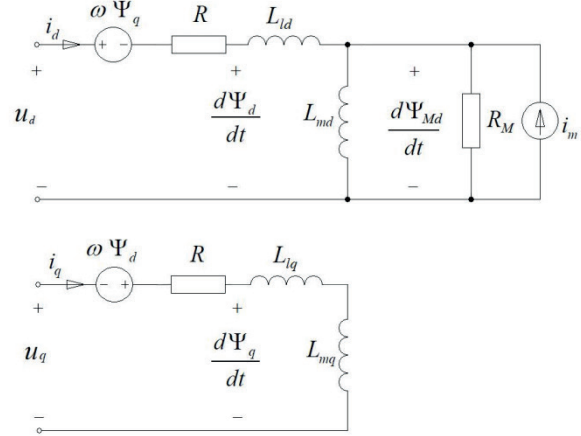


Figure 2 Equivalent circuit of the PMSM in d-axis and q-axis

Phasor diagram of the PMSM for motor operation is shown in Figure 3. The phasor diagram represents a stationary mode of operation, hence effective values for currents and voltages are used (indicated by capitals).

In Figure 3 the E_j is the phase back electromotive force (EMF), or excitation voltage, induced in the stator winding by PMs at synchronous speed (E_j depends directly on rotor speed and PM flux), I_s is the phase current, R is the stator resistance, X_{md} and X_{mq} are the d-axis and q-axis components of the synchronous reactance.

3. Electromagnetic and construction design of synchronous motor with permanent magnets on external rotor

Main results of the electromagnetic and construction design of synchronous motor with permanent magnets on external rotor is described in paper [8]. For the design and electromagnetic calculations of PMSM, the basic equations and information were used referring to [9-15]. The calculation of parameters and dimensions of SMPM was done by using a debugged m-file in MATLAB 2013a. Table 1 presents data of the designed motor. A schematic cross-section of the electromagnetic circuit with winding is presented in Figure 4.

4. FEM Simulation of SMPM with external rotor

The analytical design is validated by means of comparison to FEM simulations [8]. It was used in 2D FEM simulation that compared with 3D simulation needed a much shorter time to be calculated [16-19]. In the paper [8] presented are results from open-circuit and load simulation. The FEM simulation results correspond fairly well to the results obtained from the analytical design. The airgap flux density waveform of the machine at open-circuit simulation is presented in Figure 5. The back-EMF waveforms of the machine at open-circuit simulation are presented in Figure 6.

Table 1 Data of the PM synchronous motor [8]

Quantity	Value	Quantity	Value
rated power [W]	250	efficiency [%]	92
rated voltage [Vrms]	12	pole pieces of stator	9
rated speed [rpm]	150	pole pieces of rotor	12
outer machine diameter [mm]	160	number of coils per phase	3
total machine width [mm]	70	number of turns per coil	86
maximum torque [Nm]	20	number of winding layers	2

Table 2 Results from load simulation [8]

Quantity	Value
Peak phase current [A]	7.071
Maximum rotor iron flux density [T]	1.207
Maximum stator iron flux density [T]	1.949
Fundamental airgap flux density [T]	0.4558
Peak flux linkage, q-axis [Wb]	0.0452
Peak flux linkage, d-axis [Wb]	0.1122

Table 3 Data of simulated torque of the motor [8]

Quantity	Value
Mean airgap torque (by flux linkage and current) [Nm]	9.047
Mean airgap torque (by Maxwell stress tensor) [Nm]	9.0
Torque reduction due to iron losses [Nm]	0.1868
Torque ripple [%]	11.62

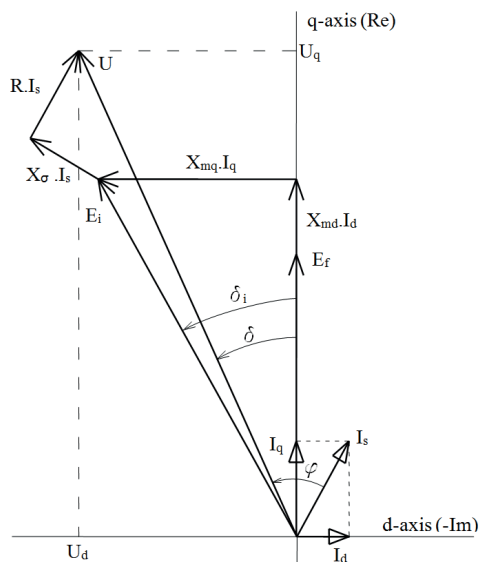


Figure 3 Phasor diagram of the PMSM in dq-axes

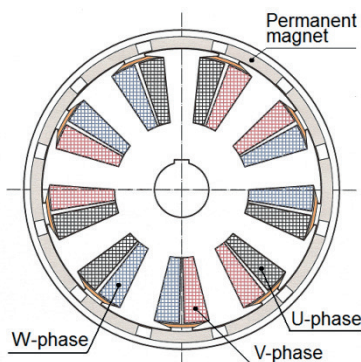


Figure 4 Electromagnetic circuit of SMPM [8]

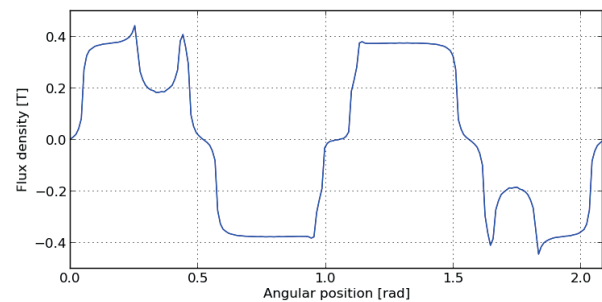


Figure 5 The airgap flux density waveform at open-circuit simulation [8]

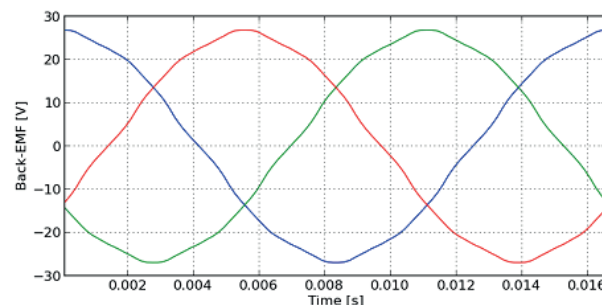


Figure 6 The back-EMF waveforms at open-circuit simulation [8]

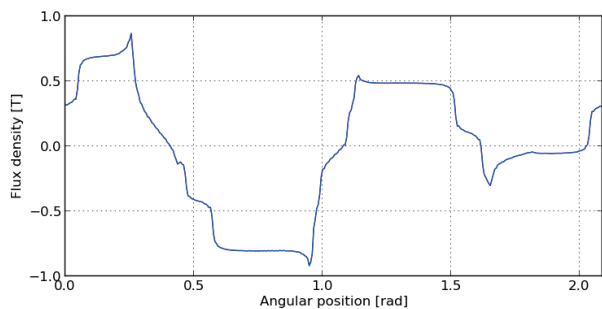


Figure 7 The airgap flux density waveform at load simulation [8]

Results from load simulation are presented in Table 2 and data for the torque motor at load simulation are presented in Table 3. The airgap flux density waveform of the machine at load

simulation is presented in Figure 7. In Figure 8 presented is torque waveform of the machine at load simulation.

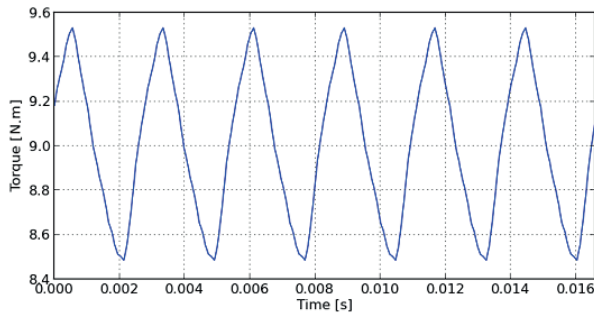


Figure 8 The torque waveform of SMPM at load simulation [8]



Figure 9 Photograph of prototype SMPM without bearing plate [8]

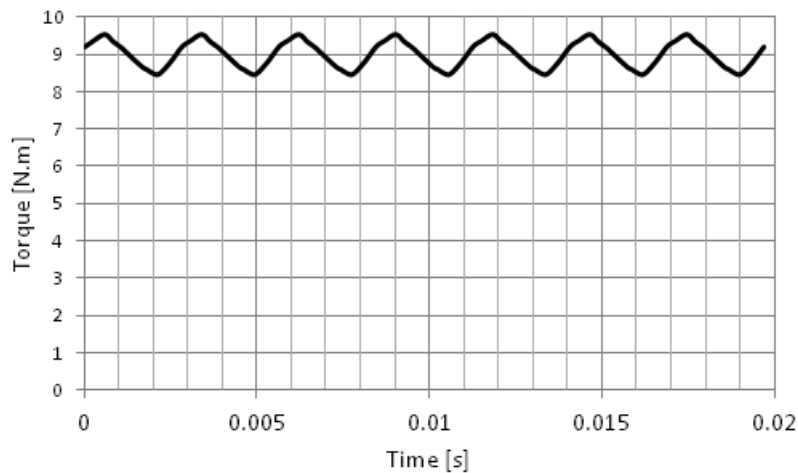


Figure 10 Torque as a function of time at the loading in motoric mode [8]

5. Prototype of SMPM with external rotor and measured results of the machine

The construction of prototype with outer rotor permanent magnet synchronous machine is described in [8] in detail. Photograph of the motor without bearing plate is shown in Figure 9.

Experimental measurements of the machine prototype were performed in laboratories. The motor was supplied from a frequency converter. Measurements of the stator quantity (voltage, current and frequency) were performed both on the frequency converter and measurement of the power on a digital wattmeter. The measurements were done in generator mode of operation for the speed of 200 rpm and for two values of speed - 120 and 200 rpm in the motor mode of operation, respectively. Measured torque ripple presented in Figure 10 is comparable with FEM simulation of torque (see Figure 8).

6. Matlab/Simulink simulation of synchronous motor with permanent magnets on external rotor

In this section presented are results of the mathematical model simulation created by Equations (4)-(10).

A) Simulation model of the permanent magnet synchronous motor

Matlab/Simulink® enables “to view” dynamic characteristics and to analyse transient performance of the motor. The

mathematical model of the permanent magnet synchronous motor, is suitable for implementation of the Matlab/Simulink method based on d,q transformations known from the reference frame theory of electrical machinery [20]. The mathematical model must correspond with the analysed motor and represents the physical phenomena as close as possible. The simulation model of the PMSM is presented in Figure 11.

The electromagnetic torque T_{em} in Fig. 11 is determined by Equation (6) and the loading torque T_L can be expressed as follows:

$$T_L = T_{em} - J \cdot \frac{d\omega_m}{dt} \quad (11)$$

where J is the rotor inertia and ω_m is angular speed of the rotor. The angular speed of the rotor is expressed by the time derivation of its displacement θ_m :

$$\omega_m = \frac{d\theta_m}{dt} \quad (12)$$

The d-q components of the armature current I_s of the PMSM (see Figure 3), in terms of the permanent magnet flux linkage Ψ_{md} and load angle δ , are introduced.

B) Simulation results

On the basis of the simulation model of PMSM (see Figure 11), the simulation of torque, speed and current characteristics has been carried out. The stator windings parameters, flux linkage

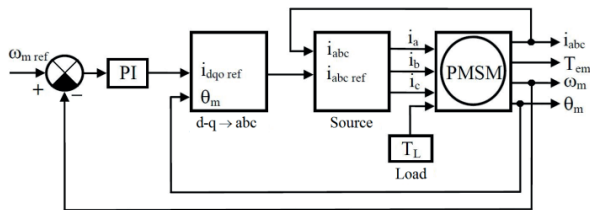


Figure 11 The simulation model of PMSM

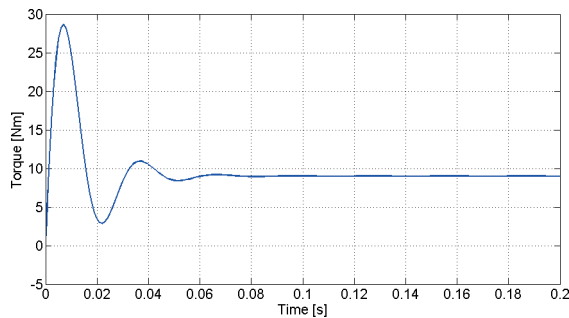


Figure 12 The dynamic torque characteristic of PMSM at rated load start-up

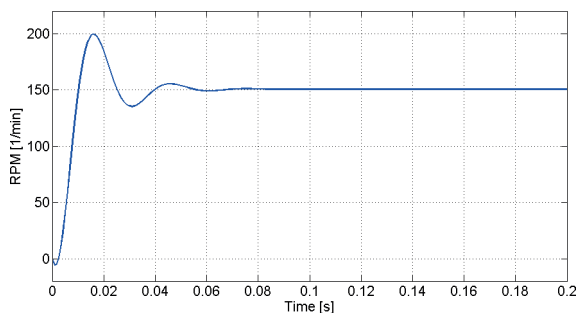


Figure 13 The mechanical speed of PMSM at rated load start-up

and synchronous d and q reactance of the motor are obtained from the FEM computations. The load torque is given as input data. The simulation procedure is performed for rated supply conditions and motor starting at the rated load $T_L = T_N$. The result of simulation torque characteristic for analyzed case is presented in Figure 12.

After the transients are suppressed, the obtained value of the simulated torque corresponds to the torque at the steady-state operating mode (see Table 3).

Figure 13 shows the mechanical speed of the PMSM. The stator currents are shown in Figures 14-16 respectively.

As it is shown in Figures 12-16, the PMSM has a good dynamic response.

7. Conclusion

The present paper describes the simulations and shows initial results of measurements of a synchronous machine prototype with an external rotor and permanent magnets. The design, FEM simulations and results of measurements are presented in paper [8].

The present paper shows the result of simulation of torque, mechanical speed and stator currents. The torque of the

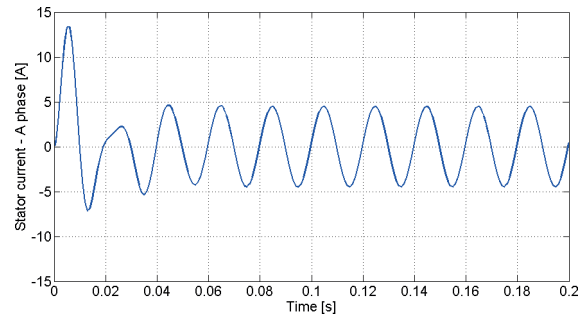


Figure 14 Motor stator current - A phase

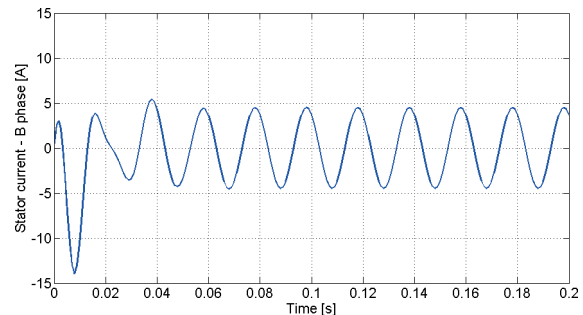


Figure 15 Motor stator current - B phase

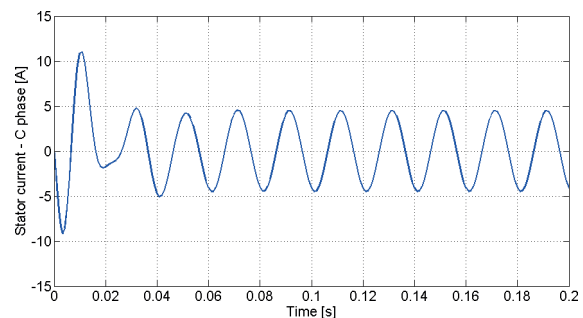


Figure 16 Motor stator current - C phase

considered PMSM in present paper is verified in three ways: simulated results in Matlab/Simulink (Figure 12) and FEM Simulation (Figure 8 and Table 3) are compared with measured value (Figure 10). Showing a very good agreement, they prove that the applied methodologies as accurate.

Mechanical properties of the prototype of the inverse synchronous motor were verified too. The SMPM was supplied from the three-phase frequency converter at the speed corresponding to operation conditions. Results of measurements obtained at the constant speed in load mode, when the inverse synchronous motor was loaded up to 130% of the nominal current, confirm suitability of inverse synchronous motor for the direct drive in-wheel operation of the electric wheelchair. On the SMPM verified have been the dynamic properties. From the results one sees that the presented inverse SMPM has good dynamic and static properties.

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